

**Electrical Engineering Department** Electronics Computers **E E E E Communications** 





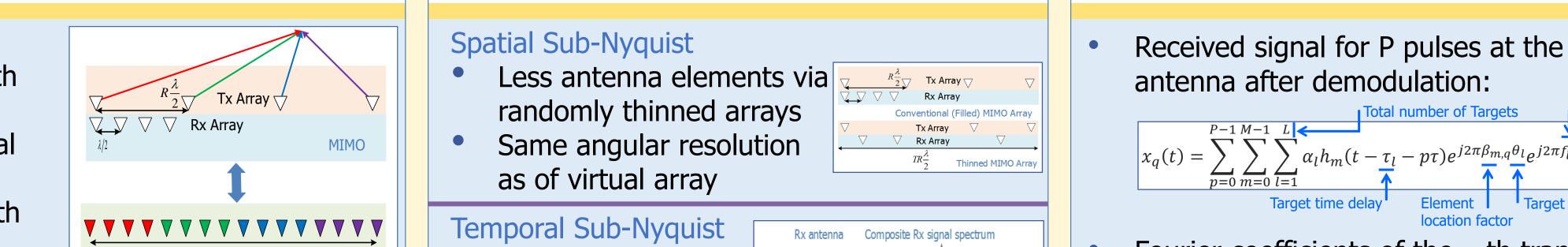
# **Cognitive Sub-Nyquist Collocated MIMO Radar Prototype** with Clutter Removal

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**Main Contributions** 

range resolution

MIMO array with Prototype realizes both spatial and fewer elements temporal sub-Nyquist sampling in a has same spatial MIMO radar without loss of angular and resolution as a virtual array with



**Conventional Collocated MIMO** 

### **Sub-Nyquist MIMO**

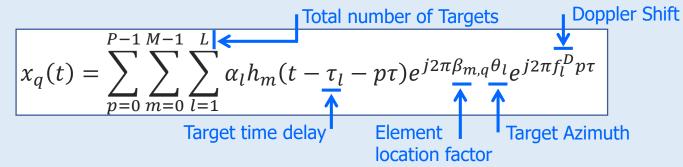
#### Spatial Sub-Nyquist

- Less antenna elements via 🔁  $R\frac{\lambda}{2}$  Tx Array randomly thinned arrays tional (Filled) MIMO Arra Tx Arrav Rx Array
- Same angular resolution as of virtual array

Thinned MIMO Array

## **Signal Model and Recovery**

Received signal for P pulses at the *q*th antenna after demodulation:



| <ul> <li>Sub-Nyquist 4x5 MIMO array shows<br/>same detection performance as Nyquist<br/>8x10 ULA</li> <li>The Reduction rate is 75%</li> <li>Cognitive transmission is employed to<br/>further enhance SNR for sub-Nyquist<br/>arrays</li> </ul>   |  |              | d to  | MIMO transmits<br>orthogonal<br>waveforms and<br>processes linear<br>combination of<br>echoes received due<br>to each waveform  | Radar cross-sect<br>antennas in co  | π       λ       Virtual array         tion is same for allocated MIMO         0       0         wirtual array       0         to array | <ul> <li>Temporal Sub-Nyq</li> <li>Reduced samp<br/>rate at each Rx</li> <li>Same range<br/>resolution as th<br/>Nyquist bandw</li> <li>Cognitive Transmis</li> <li>Entire power is<br/>in only few nar<br/>subbands</li> <li>High SNR at resolution</li> </ul> | bling<br>$f_{x}$ Echoes of<br>multiple Tx<br>waveforms<br>hat of<br>yidth TB <sub>h</sub><br>Ssion<br>focused<br>row<br>Sub-Nyquist MI   | IMO Tx Waveform   | • Fourier coefficients of the <i>m</i> th transmitter<br>channel at the <i>q</i> th receiver: Operating frequency<br>$y_{m,q}^{p}[k] = \sum_{l=1}^{L} \alpha_{l} e^{j2\pi\beta_{m,q}\theta_{l}} e^{-j\frac{2\pi}{\tau}k\tau_{l}} e^{-j2\pi f_{m}\tau_{l}} e^{j2\pi f_{l}^{D}p\tau}$ Target reflectivity<br>• Doppler focusing for a specific frequency v<br>$\varphi_{m,q}^{v}[k] = \sum_{l=1}^{L} \alpha_{l} e^{j2\pi\beta_{m,q}\theta_{l}} e^{-j\frac{2\pi}{\tau}(k+f_{m}\tau)\tau_{l}} \times \begin{cases} P &  f_{l}^{D}-\nu  < 1/2P\tau \\ e^{lse} \end{cases}$ • Use OMP for simultaneous sparse 3D recovery with focusing |
|--|--|--------------|---|---|---|---|---|--|---|---|
| Technical Specification  |  |              |   | Clutter Model   |   | Clutter Mitigation  |   | Over   | <b>Overview of Hardware Architecture</b>  |   |
| Image: Mode 1)Nyquist (Mode 3)anti-<br>(Mode 3)BW per<br>Tx (incl.<br>guard-<br>bands)15 MHz3 MHz80%The<br>randBW per<br>Tx (excl.<br>guard-<br>bands)12 MHz3 MHz75%Whe<br>at aBW per<br>Tx (excl.<br>guard-<br>bands)12 MHz3 MHz75%The<br>pointBW per<br>Tx (excl.<br>guard-<br>bands)12 MHz3 MHz75%The<br>pointBW per<br>Tx (excl.<br>guard-<br>bands)30 MHz7.5 MHz75%The<br>pointBW per<br>Tate30 MHz7.5 MHz50%The<br>point |  |              | antenna is<br>The clutter<br>range [ $\theta$ -<br>where S <sub>c</sub> ( $\theta$<br>at angle $\theta$ .<br>The delay<br>DoA $\phi_c \sim$ | ved signal $r_q(t)$ at the $a_{s} r_q(t) = x_q(t) + y_q(t) + n_q(t)$<br>er amplitude in the angu-<br>$\epsilon, \theta + \epsilon$ ) is<br>$\left[a_c = \frac{1}{2\pi} \int_{\theta-\epsilon}^{\theta+\epsilon} S_c(\theta) d\theta\right]$ $\theta$ is the clutter amplitu<br>$a_c \sim N(a_c, \sigma_c^2)$<br>S $\tau_c \sim U(0, \tau)$ ,<br>$\tau U(-1, 1)$ and<br>ppler spectrum $\nu_n \sim N(\nu_c)$ | (t)<br>ular<br>de density   | r m is number of Transmitters<br>P is number of pulses<br>Q is number of receivers<br>K is randomly chosen group of coefficients<br>$ \frac{Four \text{ stages for clutter whitening}}{I. Subtracting the mean :} R_m^T - E[Y_m^T + N_m^T] \text{ or } \tilde{R}_m = X_m^T + \tilde{Z}_m$ 1. Subtracting the mean :<br>$R_m^T - E[Y_m^T + N_m^T] = X_m^T + Z_m^T - E[Y_m^T + N_m^T] \text{ or } \tilde{R}_m = X_m^T + \tilde{Z}_m$ 2. Reshaping : $\tilde{Z}_m$ is reshaped from a $P \times KQ$ matrix<br>to $PQ \times K$ matrix or $\hat{Z}_m$ is a $PO \times K$ clutter-plus-noise<br>matrix. $\tilde{R}_m$ is reshaped to $\hat{R}_m$ 3. Whitening : The covariance matrix of the $q^{th}$ column $\hat{z}_{pq,k}$ of $\hat{Z}_m$<br>is a $PQ \times PQ$ .<br>Toeplitz matrix: $D_m = E[\hat{z}_{pq,k}\overline{\hat{z}_{pq,k}}]$   |   |  | Laptop/PC<br>User<br>Interface<br>S <sub>r</sub> [n] = I <sub>r</sub> [n] -<br>(serializ<br>Modes 1, 2 and 4<br>Mode 3<br>Spectrum of |   |
| Array Modes  |  |              |   | Waveform Generator  |   |   | Analog Pre-Processor (APP)  |  |   | <b>Digital Receiver</b>   |
| Mode 1: 8x<br>Filled uniform<br>Mode 2: 8x<br>Filled random<br>Mode 3: 4x<br>Thinned random<br>(~Virtual 8x10<br>Spatial sub-Ny<br>Mode 4: 8x<br>Thinned random<br>(~Virtual 20x2)   | n array<br>x10<br>n array<br>4x5<br>m array<br>0 ULA)<br>0<br>lyquist<br>x10<br>x10<br>x10<br>x10<br>0 | ° X ∞<br>0.5 | x x x $x x$ $x x$ $x x$ $x x$ $x x$ $x x$ $x$ $x$ $x$ $x$ $x$ $x$ $x$ $x$ $x$   | <ul> <li>Total BW, 8 Tx: 12<br/>3 MHz guard-band</li> <li>Eight 375 kHz cog<br/>slices per Tx</li> <li>Cognitive BW, 1 Tx<br/>3 MHz (= 8 x 375)</li> <li>BW reduction, 1 Tx<br/>(excl. guard-bands<br/>75% (3 of 12 Mhz)</li> </ul>   | SimulationXilinx VNitiveImage: State of the |   | <ul> <li>APP card in a single chassis</li> <li>BPFs have ~30</li> </ul>   | Input       Splitter       10dB       BF         Input       Input       Input       Input       Input         0.5-120MHz       Input       Input       Input       Input         Input       Input       Input< |   | <ul> <li>Two 16-bit eight-<br/>channel digitizers<br/>for I and Q<br/>streams</li> <li>Sub-Nyquist<br/>sampling rate: 7.5<br/>MHz/channel</li> <li>Signal BW with<br/>guard-bands: 30<br/>MHz/channel</li> </ul>  |
|  |  |              | Sample Measurements Decults   |   |   |   |   |  |   |   |

User Interface \ Radar Display

#### **Sample Measurements Results**

